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This application is related to the patent application entitled “SPECKLE BASED SENSOR FOR THREE DIMENSIONAL NAVIGATION” Attorney Docket Number 10030719 filed on the same day and assigned to the same assignee.

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The invention relates to increasing the light collection efficiency of photodetector arrays using lightpipe or reflector technology.

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Speckle patterns are interference patterns emitted from target surfaces illuminated by coherent light. If the target surface moves, the associated speckle pattern is moved as well. This physical phenomenon provides the basis for speckle based navigation sensors. Typically, speckle based navigation sensors include a laser light source, optical components and a photodetector. The speckle pattern consists of speckle “beams” that are emitted nearly isotropically from the illuminated target

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surface

The speckle pattern emitted from an illuminated target surface is made up of quasi-collimated beams of light. The cross sectional diameter of an individual speckle beam is inversely proportional to the diameter of the illuminated spot on the target surface and is proportional to the distance from the target surface. Typically,

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two photodetector arrays are used in speckle based navigation sensors with each

photodetector array sensing motion along one of the axes, respectively. The cross sectional speckle beam size must be matched to the size of the individual photodetector array elements. Hence, the photodetector arrays or collection optics are often positioned at relatively large distances from the target surface and therefore
5 subtend small angles from the target surface. Because speckle “beams” propagate away from the target surface in nearly an isotropic pattern, only a relatively small fraction reaches the photodetector array. This limits the performance of speckle based navigation sensors.

FIG. 1 shows a conceptual view of a conventional speckle based navigation
10 sensor system for two dimensional navigation. Photodetector arrays 120 and 125 detect a fraction of speckle beams 165 from target surface 135. For example, if photodetector arrays 120 and 125 are located approximately 20 mm from target surface 135 illuminated by the laser light, the angles subtended by photodetector arrays 120 and 125 from target surface 135 are about 7 x 24 degrees. Because speckle
15 is emitted nearly isotropically only about 1% of the speckle flux strikes photodetector arrays 120 and 125, assuming a photodetector array area of 2.8 x 8.6 mm.

Summary of the Invention

In accordance with the invention, lightpipe and reflector technology is used to
20 increase collection efficiency in speckle based navigation sensors. Increasing the collection efficiency improves the optical performance of speckle based navigation sensors and also allows reduction in the photodetector size at the price of decreased collection efficiency. Smaller photodetector size typically reduces the photodetector cost.

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Brief Description of the Drawings

FIG. 1 shows prior art speckle based navigation sensor.

FIG. 2a shows the use of a lightpipe in accordance with the invention to improve collection efficiency of a speckle based optical navigation sensor.

- 5 FIG. 2b shows an embodiment of a lightpipe in accordance with the invention where the area of the top face has been increased by slanting it at an angle with respect to the bottom face.

FIG. 3 shows the use of an elliptical reflector in accordance with the invention to improve collection efficiency of a speckle based optical navigation sensor.

- 10 FIG. 4 shows the effect of undesirable boundary reflections in accordance with the invention.

FIG. 5 shows the use of a lightpipe in accordance with the invention having elliptical sidewalls to improve collection efficiency of a speckle based optical navigation sensor.

- 15 FIG. 6 shows the use of a lightpipe in accordance with the invention having elliptical sidewalls and microstructure to improve collection efficiency of a speckle based optical navigation sensor.

FIG. 7 shows a simplified view of a speckle based optical navigation system having improved collection efficiency in accordance with the invention.

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Detailed Description of the Invention

- FIG. 2a shows an embodiment in accordance with the invention. Lightpipe 210 is positioned between target surface 235 and photodetector array 220. Lightpipe 210 is made from a transparent material such as, for example, acrylic with a refractive
- 25 index in the range from about 1.5 to 1.6 or SiO₂ to enhance the refractive index

contrast with the surrounding medium, typically air. Introduction of lightpipe 210 significantly improves the collection efficiency of speckle beams 265. Photodetector array 220 is positioned directly beneath lightpipe 210. Speckle beams 265 from target surface 235 strike the top of lightpipe 210 and are refracted into the interior. Many speckle beams 265 propagating away from photodetector array 220 are redirected to strike photodetector array 220 by total internal reflection within lightpipe 210. Sides 202 and 203 of lightpipe 210 are typically absorptive to prevent reversal of the apparent motion of the speckle pattern as described below with reference to FIG. 4. Use of lightpipe 210, for example, allows photodetector array 220 with an area of 0.75 x 2 mm to collect about 11% of speckle beams 265 compared with larger photodetector array 120 that collects only about 1% of speckle beams 165 .

FIG. 2b shows an embodiment in accordance with the invention. Lightpipe 250 is similar to lightpipe 210 but top face 275 is inclined at suitable angle with respect to bottom face 265 in FIG. 2b in order to increase the light gathering area available. Hence, speckle beams 265 that would not be incident on lightpipe 210 are captured by lightpipe 250 because of the larger surface area of top face 275.

FIG. 3 shows an embodiment in accordance with the invention using elliptical reflector 350 to improve the collection efficiency of speckle beams 365. Sidewalls 351 and 352 of elliptical reflector 350 have an elliptical cross-section that is swept in one direction. Optically, an ellipse has the property that that any light ray passing through one focus of the ellipse is reflected towards the second focus of the ellipse. For elliptical sidewalls 351 and 352, the locus of focal points forms two focal lines; one proximate to the bottom of elliptical sidewalls 351 and 352 and one proximate to top of elliptical sidewalls 351 and 352 in FIG. 3. The locus of focal points is also known as the blur spot. By centering target surface 335 on the top focal line of

elliptical sidewalls 351 and 352 and centering photodetector array 320 on the bottom focal line, speckle beams 365 striking elliptical sidewalls 351 or 352 are reflected to strike photodetector array 320. Typical coatings for elliptical sidewalls are aluminum, silver and gold. Such metallic high reflectivity coatings typically contain a dielectric overcoat to prevent oxidation. High reflectivity dielectric coatings may also be used. The collection efficiency using reflector 350 is about 9% which is almost about an order of magnitude better than the conventional embodiment in FIG. 1.

The two remaining sidewalls (sidewalls 475 and 480 in FIG. 4) of reflector 310 are planar and typically are absorptive. Typically, sidewalls 475 and 480 may be made absorptive by application of a black wax or black tape. Black wax is typically a wax with carbon particulates in it. Alternatively, the two remaining sides of reflector 310 may be open. The reason for this is illustrated in FIG. 4 showing a view of reflector 310. When speckle beams 365 (see FIG. 3) are reflected in a direction predominantly perpendicular to detector elements 410 of photodetector array 320, the apparent motion of the speckle pattern is reversed. The apparent motion of speckle pattern 430 is initially in the direction of sidewall 475 but upon reflection from sidewall 475, the apparent motion of speckle pattern 430 is reversed and towards sidewall 480. Hence, only speckle beams 365 reflected in directions predominantly parallel to detector elements 410 of photodetector array 320 provide desirable signals for tracking the apparent motion of speckle patterns. Providing planar sidewalls located some distance from photodetector array 320 also reduces the amount of speckle beams 365 (see FIG. 3) reflected back to photodetector array 320 from the planar sidewalls.

FIG. 5 shows lightpipe 500 having elliptical sidewalls 551 and 552. FIG. 5 is similar to FIG. 2a but has elliptically shaped sidewalls similar to FIG. 3. Hence

lightpipe 500 is made from a transparent material such as, for example, acrylic with a refractive index in the range from about 1.5 to 1.6 or SiO₂. Sidewalls 551 and 552 are elliptical and form the interface from the transparent material to air or another material having a different refractive index so that there is a refractive index change

5 along elliptical sidewalls 551 and 552. The planar sidewalls of lightpipe 500 are typically optically absorptive to prevent reversal of the apparent motion of the speckle pattern as described above with reference to FIG. 4. Target surface 535 is typically positioned a small distance away from lightpipe 500 so that most of the speckle beams strike at or near the top focal line of elliptical side walls 551 and 552 in FIG. 5. These

10 speckle beams are then refracted into lightpipe 500. Speckle beams not refracted towards photodetector array 520 undergo total internal reflection from elliptical sidewalls 551 and 552 and are reflected toward the bottom focal line or blur spot. This increases the collection efficiency on photodetector array 520 to about 11.5%.

FIG. 6 shows lightpipe 600 having elliptical sidewalls 651 and 652 similar to lightpipe 500 in FIG. 5 but also having microstructure fabricated into lightpipe 600 to

15 further enhance collection efficiency. Typically, the microstructure is a diffraction grating such as diffraction grating 680. The periodicity of diffraction grating 680 is designed such that the periodicity decreases with increasing distance from the center axis of lightpipe 600 according to the formula

20 $\sin \theta_{incident} - n_{lightpipe} \sin \theta_{diffraction} = \pm m \lambda / \Lambda$ where Λ is the grating periodicity, m is an integer typically set to 1, $\theta_{incident}$ is the angle of incidence onto diffraction grating 680, $\theta_{diffraction}$ is the diffraction angle and $n_{lightpipe}$ is the index of refraction of lightpipe 600. Speckle 675 incident on diffraction grating 680 from target surface 635 is then diffracted towards photodetector array 620 instead of being lost out of the two non-

25 elliptical sidewalls of lightpipe 600. The collection efficiency on photodetector array

620 is improved to about 28%. Similarly, the embodiment in accordance with the invention in FIG. 3 may include a diffraction grating at the top focal line of elliptical sidewalls 351 and 352 opposite photodetector array 320.

FIG. 7 shows a simplified view of using a lightpipe in the context of speckle based optical navigation sensor in accordance with the invention. Coherent light source 705 is positioned off center with respect to lens 710 so that target surface area 735 may be illuminated. Note that lens 710 may be replaced by, for example, a grating without changing the basic operation. Hence light beam 755 is directed at an angle towards surface 740 to illuminate target surface area 735. Speckle pattern 780 is scattered into light collector 700 for collection at photodetector array 725. Embodiments of light collector 700 includes any of the embodiments in accordance with the invention discussed herein such as lightpipe and reflector light collectors.

While the invention has been described in conjunction with specific embodiments, it is evident to those skilled in the art that many alternatives, modifications, and variations will be apparent in light of the foregoing description. Accordingly, the invention is intended to embrace all other such alternatives, modifications, and variations that fall within the spirit and scope of the appended claims.

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